

Problem 1

$$I(s) = \left(\frac{1}{R} + \frac{1}{Ls} + Cs \right) V(s)$$

$$I(s) = \left(\frac{Ls + R + RLCs^2}{RLs} \right) V(s)$$

$$\frac{V(s)}{I(s)} = \frac{RLs}{Ls + R + RLCs^2}$$

$$\frac{V(s)}{I(s)} = \frac{\frac{1}{Cs}}{s^2 + \frac{1}{RC}s + \frac{1}{LC}}$$

Problem 2

For writing the differential equation for the displacement x_1 of mass m_1 apply the super position principle, m_1 moving m_2 stationary

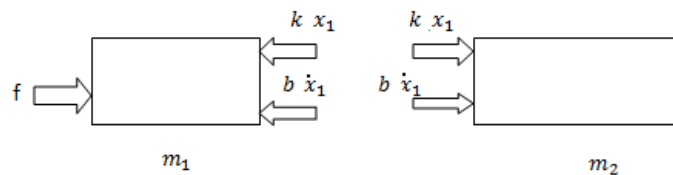


Figure 1: Free Body Diagram of Spring-Mass-Damper System m_1 moving m_2 stationary

Using free body diagram, equation of motion for m_1 according to Newton's second law is

$$F_{net} = m_1 a = f - (x_1 - x_2)k - (\dot{x}_1 - \dot{x}_2)b$$

$$(m_1 s^2 + bs + k)X_1(s) + (-bs - k)X_2(s) = F(s) \quad (2.1)$$

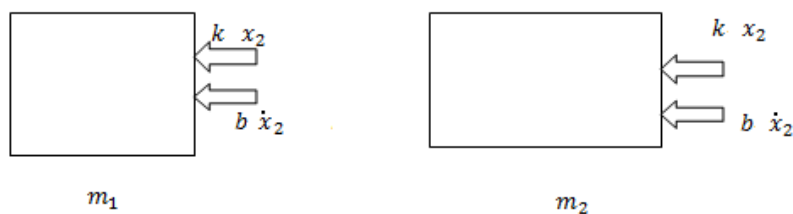


Figure 2: Free Body Diagram of Spring-Mass-Damper System m_2 moving m_1 stationary

For writing the differential equation for the displacement x_2 of mass m_2 apply the super position principle, m_2 moving m_1 stationary

$$\begin{aligned} m_2 \ddot{x}_2 &= b\dot{x}_1 + kx_1 - b\dot{x}_2 - kx_2 \\ m_2 \ddot{x}_2 + b(\dot{x}_2 - \dot{x}_1) + k(x_2 - x_1) &= 0 \\ (-bs - k)X_1(s) + (m_2s^2 + bs + k)X_2(s) &= 0 \end{aligned} \tag{2.2}$$

Eq(2.1) \times $(-bs - k)$ - Eq(2.2) \times $(m_1s^2 + bs + k)$

$$(bs + k)^2 X_2(s) - (m_1s^2 + bs + k)(m_2s^2 + bs + k)X_2(s) = F(s)(-bs - k)$$

$$\begin{aligned} X_2(s) &= \frac{bs + k}{(m_1s^2 + bs + k)(m_2s^2 + bs + k) - (bs + k)^2} \\ &= \frac{bs + k}{m_1m_2s^4 + (m_1 + m_2)bs^3 + (m_1 + m_2)ks^2} \\ \frac{X_2(s)}{F(s)} &= \frac{\begin{vmatrix} m_1s^2 + k + bs & F(s) \\ -(k + bs) & 0 \end{vmatrix}}{\begin{vmatrix} m_1s^2 + k + bs & -(k + bs) \\ -(k + bs) & m_2s^2 + k + bs \end{vmatrix}} \\ \frac{X_2(s)}{F(s)} &= \frac{bs + k}{(m_1s^2 + bs + k)(m_2s^2 + bs + k) - (bs + k)^2} \end{aligned}$$

Problem 3

$$\begin{aligned} \frac{dy}{dt} + 10(1 - y) &= 2x \\ \frac{dy}{dt} - 10y + 10 &= 2x \end{aligned}$$

Let $u = 2x - 10$

$$\frac{T(s)}{U(s)} = \frac{1}{s - 10}$$

Problem 4

$$\begin{aligned} x &= \begin{bmatrix} \dot{y} \\ \theta \\ \dot{\theta} \end{bmatrix} \\ \begin{bmatrix} \ddot{y} \\ \ddot{\theta} \\ \ddot{\theta} \end{bmatrix} + \begin{bmatrix} 0 & \frac{-mg}{M} & 0 \\ 0 & 0 & 1 \\ 0 & \frac{g}{l} & 0 \end{bmatrix} \begin{bmatrix} \dot{y} \\ \theta \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} \frac{1}{M} \\ 0 \\ \frac{-1}{Ml} \end{bmatrix} u \\ y &= \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \dot{y} \\ \theta \\ \dot{\theta} \end{bmatrix} \end{aligned}$$

Problem 5

$$\begin{aligned}\frac{Y(s)}{U(s)} &= C(sI - A)^{-1}B + D \\ (sI - A)^{-1} &= \begin{bmatrix} s & 1 \\ -1 & s \end{bmatrix}^{-1} = \frac{1}{s^2 + 1} \begin{bmatrix} s & -1 \\ 1 & s \end{bmatrix} \\ \frac{Y(s)}{U(s)} &= \frac{1}{s^2 + 1} \begin{bmatrix} -1 & 0 \end{bmatrix} \begin{bmatrix} s & -1 \\ 1 & s \end{bmatrix} \begin{bmatrix} 1 \\ -1 \end{bmatrix} + 1 \\ &= \frac{1}{s^2 + 1} \begin{bmatrix} -1 & 0 \end{bmatrix} \begin{bmatrix} s + 1 \\ 1 - s \end{bmatrix} + 1 \\ &= \frac{s(s + 1)}{s^2 + 1}\end{aligned}$$

Problem 6

$$\begin{aligned}Y(s) &= G(s)\frac{1}{s} = \frac{s - 1}{s(s + 1)(s + 2)} \\ &= \frac{-1}{s} + \frac{2}{s + 1} + \frac{-3}{s + 2} \\ y(t) &= \frac{-1}{2} + 2e^{-t} - \frac{3}{2}e^{-2t}\end{aligned}$$

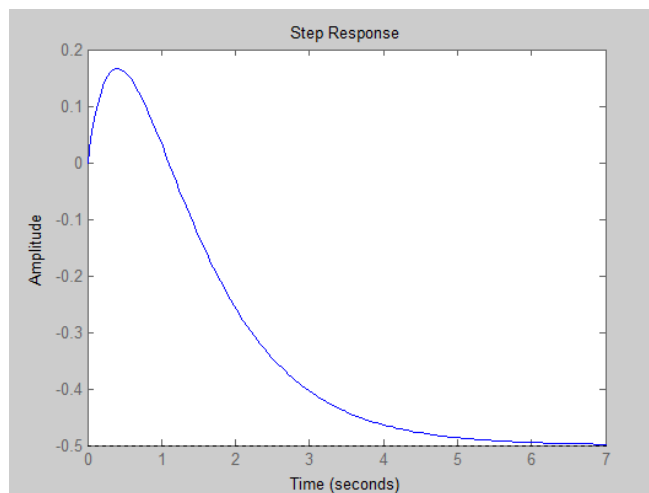


Figure 3

Problem 7

$$G_1(s) = \frac{4}{s + 4}, G_2(s) = \frac{2}{s + 2}$$

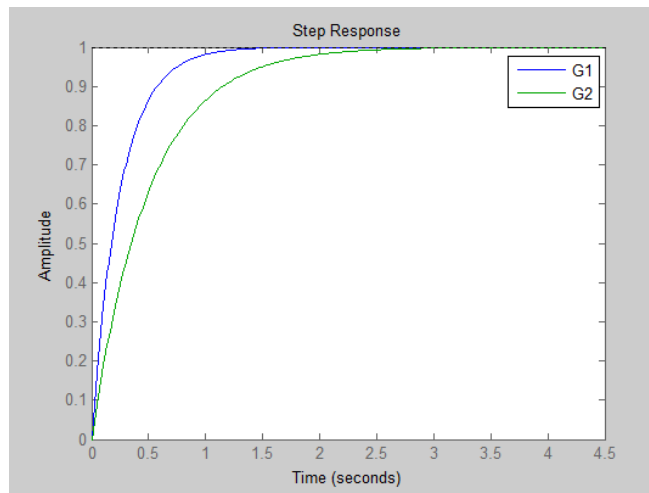


Figure 4

Problem 8

$$\begin{aligned}
 g(\infty) &= \lim_{s \rightarrow 0} sG(s) = \lim_{s \rightarrow 0} \frac{20}{s^2 + 5s + k} \\
 &= \frac{20}{k} = 10 \\
 k &= \frac{20}{10} = 2
 \end{aligned}$$

Problem 9

$$\begin{aligned}
 s^2 + 10s + 75 &= 0 \\
 s &= -5 \pm 5\sqrt{2}j
 \end{aligned}$$

Response of the system is under-damped.

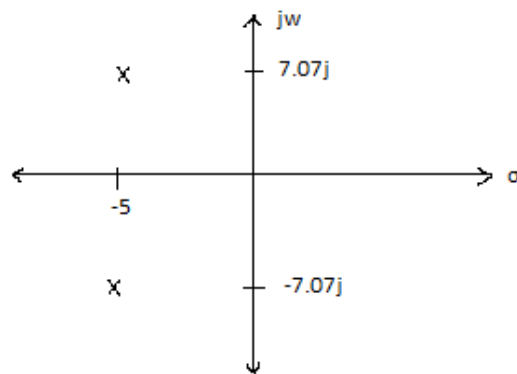


Figure 5

Problem 10

First consider the second order system only

$$G(s) = \frac{150}{s^2 + 10s + 75}$$

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For this second order system settling time is:

$$t_s = \frac{4}{\sigma_d} = \frac{4}{5} = 0.8 \text{ sec}$$

According to second order proximity criteria we have to place third pole as:

$$p > 5(\sigma_d) = 5(5) = 25$$

Let $p = 30$

Problem 11

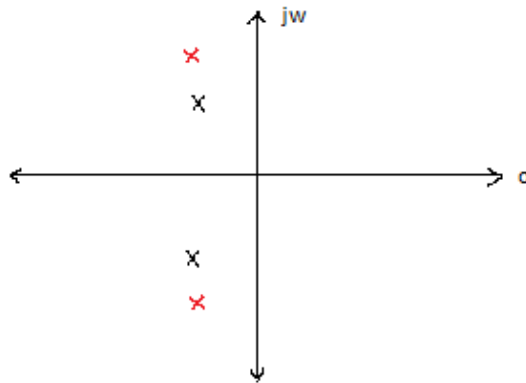


Figure 6



Figure 7

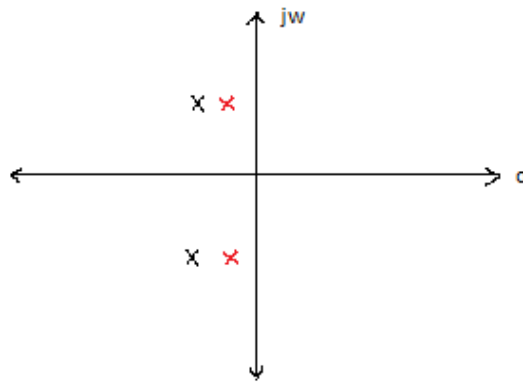


Figure 8

Problem 12

$$r(t) = \cos(2t)$$

Problem 13

Applying Routh-Hurwitz criterion to the denominator of transfer function. The routh table is given by

s^3	1	4	0
s^2	3	$k+1$	0
s^1	$\frac{12-(k+1)}{3}$	0	0
s^0	20	0	0

For the system to be BIBO stable all poles should be in left half plane it means there must be no sign change in first column of the table so:

$$\frac{12 - (k + 1)}{3} > 0$$

$$k + 1 < 12$$

$$k < 11 \tag{13.1}$$

$$k + 1 > 0$$

$$k < -1 \tag{13.2}$$

From Eq(13.1) and Eq(13.2)

$$-1 < k < 11$$

Problem 14

$$\begin{aligned} \frac{Y(s)}{R(s)} &= \frac{KG(s)}{1 + KG(s)} \\ &= \frac{K}{1 + \frac{K}{s^3 + 3s^2 + 4s + 1}} \end{aligned}$$

$$= \frac{K}{s^3 + 3s^2 + 4s + K + 1}$$

$$E(s) = (1 - Y(s))R(s)$$

$$= \left(\frac{s^3 + 3s^2 + 4s + 1}{s^3 + 3s^2 + 4s + K + 1} \right) \frac{1}{s}$$

$$e(\infty) = \lim_{s \rightarrow 0} sE(s) = \frac{1}{K + 1} < 0.1$$

$$K + 1 > 10$$

$$K > 9$$

But for stability $K < 11$ so:

$$9 < K < 11$$

Problem 15

$$\tau \approx 0.7$$

$$\sigma \approx \frac{1}{0.7} \approx 1.4$$

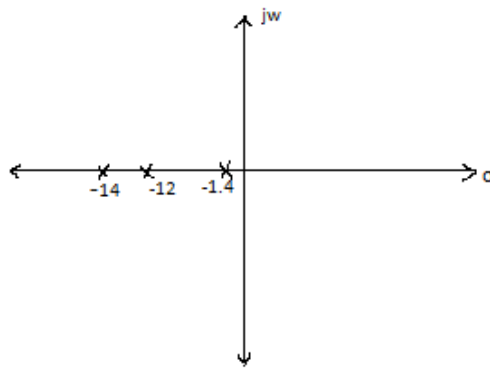


Figure 9